



**High-Temperature Precision Hall-Effect Switch** 

## FEATURES AND BENEFITS

- Unipolar switchpoints
- ASIL A functional safety compliance
- Automotive-grade ruggedness and fault tolerance
   Extended AEC-Q100 qualification
  - □ Reverse-battery and 40 V load dump protection
  - $\Box$  Operation from -40°C to 175°C junction temperature
  - □ High EMC immunity, ±12 kV HBM ESD
  - □ Output short-circuit and overvoltage protection
  - □ Superior temperature stability
- Resistant to physical stress
- Operation from unregulated supplies, 2.8 to 24 V
- Chopper stabilization
- Solid-state reliability
- · Industry-standard packages and pinouts

### PACKAGES:



## DESCRIPTION

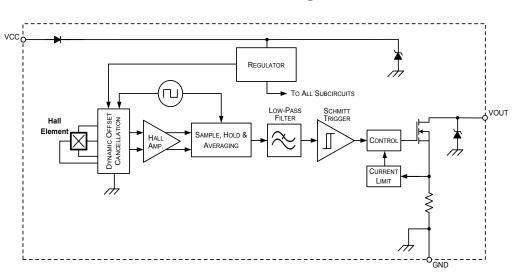
The APS11200 is a three-wire, planar Hall-effect sensor integrated circuit (IC). This device was developed in accordance with ISO 26262 and supports a functional safety level of ASIL A.

This Hall-effect switch IC features extended AEC-Q100 qualification and is ideal for high-temperature operation up to 175°C junction temperatures. In addition, the APS11200 includes a number of features designed specifically to maximize system robustness such as reverse-battery protection, output current limiter, overvoltage, and EMC protection.

The single silicon chip includes: a voltage regulator, a Hall plate, small signal amplifier, chopper stabilization, Schmitt trigger, and a short-circuit-protected open-drain output. A south pole of sufficient strength turns the output on. Removal of the magnetic field—or a north pole—turns the output off. The devices include on-board transient protection for all pins, permitting operation directly from a vehicle battery or regulator with supply voltages from 2.8 to 24 V.

Two package styles provide a choice of through-hole or surface mounting. Package type LH is a modified SOT23W, surfacemount package, while UA is a three-lead ultra-mini SIP for through-hole mounting. Both packages are lead (Pb) free and RoHs compliant with 100% matte-tin leadframe plating.

### **Functional Block Diagram**



### **SELECTION GUIDE**

Part Number	Packing <sup>[1]</sup>	Mounting	Branding	Ambient, T <sub>A</sub>	Switchpoints (Typ.)	
					B <sub>OP</sub>	B <sub>RP</sub>
APS11200LLHALX	13-in. reel, 10000 pieces/reel 3-pin SOT23W surface mount A21					
APS11200LLHALT <sup>[2]</sup>	7-in. reel, 3000 pieces/reel	3-pin SOT23W surface mount	A21	–40°C to 150°C	35 G	25 G
APS11200LUAA	Bulk, 500 pieces/bag	3-pin SIP through hole	A22			

<sup>[1]</sup> Contact Allegro for additional packing options.

<sup>[2]</sup> Available through authorized Allegro distributors only.



### **ABSOLUTE MAXIMUM RATINGS**

Characteristic Sy		Notes	Rating	Units
Forward Supply Voltage [1] V <sub>CC</sub>			30	V
Reverse Supply Voltage [1]	V <sub>RCC</sub>		-18	V
Output Off Voltage <sup>[1]</sup>	V <sub>OUT</sub>		30	V
Output Current <sup>[2]</sup>	I <sub>OUT</sub>		60	mA
Reverse Output Current	I <sub>ROUT</sub>		-50	mA
Magnetic Flux Density <sup>[3]</sup>	В		Unlimited	-
Marian In the Tanana tan	T (m m)		165	°C
Maximum Junction Temperature	T <sub>J</sub> (max)	For 500 hours	175	°C
Storage Temperature	T <sub>stg</sub>		-65 to 170	°C
	V <sub>ESD(HBM)</sub>	AEC-Q100, Human Body Model	±12	kV
ESD Voltage <sup>[4]</sup>	V <sub>ESD(CDM)</sub>	AEC-Q100, Charged Device Model	±1	kV
	V <sub>ESD(SYS)</sub>	ISO 10605, System Level	±15	kV

<sup>[1]</sup> This rating does not apply to extremely short voltage transients such as load dump and/or ESD. Those events have individual ratings, specific to the respective transient voltage event.

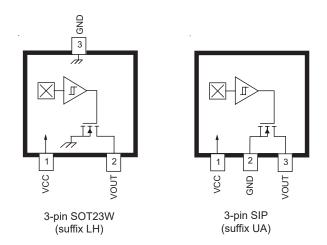
<sup>[2]</sup> Through short-circuit current limiting device.

[3] Guaranteed by design.

<sup>[4]</sup> System level ESD performance based on use with the application circuit shown in Figure 4 and the 2 k $\Omega$ /330 pF ESD discharge network.



## PINOUT DIAGRAMS AND TERMINAL LIST



#### **Terminal List**

Nome	Description	Number		
Name	Description	LH	UA	
VCC	Connects power supply to chip	1	1	
VOUT	Output from circuit	2	3	
GND	Ground	3	2	

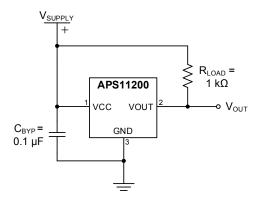


Figure 1: Typical Application Circuit



## **High-Temperature Precision Hall-Effect Switch**

#### **ELECTRICAL CHARACTERISTICS:** Valid over full operating voltage, ambient temperature range $T_A = -40^{\circ}$ C to 150°C, and with $C_{BVP} = 0.1 \,\mu$ F, unless otherwise specified

Characteristics	Symbol	Test Conditions	Min.	Typ. <sup>[1]</sup>	Max.	Unit <sup>[2]</sup>
ELECTRICAL CHARACTERISTICS	;					
Forward Supply Voltage	V <sub>CC</sub>	Operating, T <sub>J</sub> < 175°C	2.8	_	24	V
Supply Current	I <sub>CC</sub>		1	2	3	mA
Output Leakage Current	IOUTOFF	V <sub>OUTOFF</sub> = 24 V, B < B <sub>RP</sub>	-	_	10	μA
Output Saturation Voltage	V <sub>OUT(SAT)</sub>	I <sub>OUT</sub> = 20 mA, B > B <sub>OP</sub>	-	200	500	mV
Output Off Voltage	V <sub>OUTOFF</sub>	B < B <sub>RP</sub>	-	_	24	V
Power-On Time	t <sub>ON</sub>	$V_{CC} \ge V_{CC}(min)$ , B < B <sub>RP</sub> (min) – 10 G, B > B <sub>OP</sub> (max) + 10 G	_	_	25	μs
Power-On State, Output <sup>[3]</sup>	POS	$V_{CC} \ge V_{CC}(min), t < t_{ON}$		Low		-
Chopping Frequency	f <sub>C</sub>		-	800	_	kHz
Output Rise Time <sup>[4]</sup>	t <sub>r</sub>	$R_{LOAD} = 1 \text{ k}\Omega, C_L = 20 \text{ pF}$	-	0.2	2	μs
Output Fall Time <sup>[4]</sup>	t <sub>f</sub>	$R_{LOAD} = 1 k\Omega, C_{L} = 20 pF$	-	0.1	2	μs
TRANSIENT PROTECTION CHARA	ACTERISTICS					
Output Short-Circuit Current Limit	I <sub>OM</sub>		30	_	60	mA
Output Zener Clamp Voltage	V <sub>Zoutput</sub>	$I_{OUTOFF} = 3 \text{ mA}; T_A = 25^{\circ}\text{C}, \text{ Output Off}$	30	-	_	V
Reverse Battery Current	I <sub>RCC</sub>	V <sub>RCC</sub> = -18 V, T <sub>A</sub> = 25°C	-	-	-5	mA
Supply Zener Clamp Voltage	Vz	$I_{CC} = I_{CC}(max) + 3 \text{ mA}, T_{A} = 25^{\circ}C$	30	-	_	V
MAGNETIC CHARACTERISTICS			·			
Operate Point	B <sub>OP</sub>		_	35	50	G
Release Point	B <sub>RP</sub>		5	25	_	G
Hysteresis	B <sub>HYS</sub>	$(B_{OP} - B_{RP})$	7	10	20	G

 $^{[1]}$  Typical data are at  $T_A$  = 25°C and  $V_{CC}$  = 12 V.  $^{[2]}$  1 G (gauss) = 0.1 mT (millitesla).

<sup>[3]</sup> Guaranteed by device design and characterization.

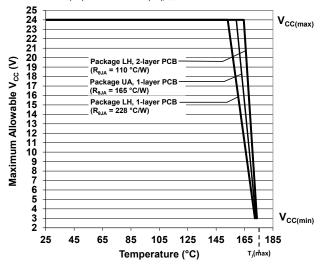
 $^{[4]}C_L$  = oscilloscope probe capacitance.



## **High-Temperature Precision Hall-Effect Switch**

### THERMAL CHARACTERISTICS: May require derating at maximum conditions; see application information

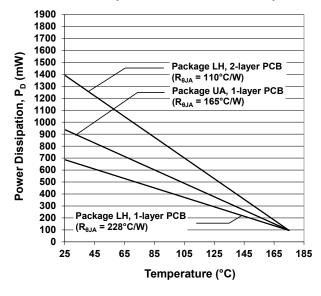
Characteristic	Characteristic Symbol Test Conditions		Value	Units
Package Thermal Resistance		Package LH, 1-layer PCB with copper limited to solder pads		°C/W
	$R_{\theta JA}$	Package LH, 2-layer PCB with 0.463 in? of copper area each side connected by thermal vias	228 110	°C/W
		Package UA, 1-layer PCB with copper limited to solder pads	165	°C/W



### Power Derating Curve

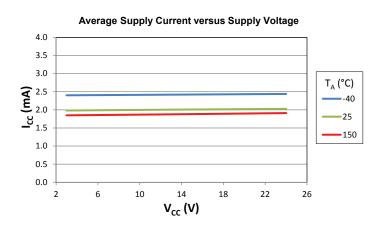
 $T_{J(max)} = 175^{\circ}C; I_{CC} = I_{CC(max)}, I_{OUT} = 0 \text{ mA (Output Off)}$ 

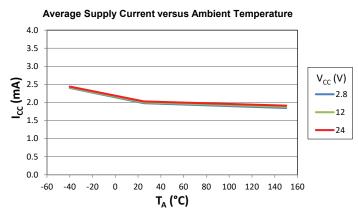
#### **Power Dissipation versus Ambient Temperature**

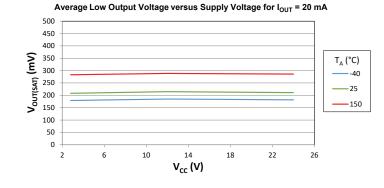




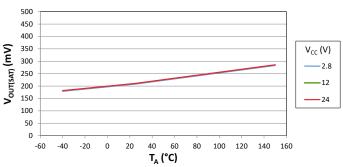
### CHARACTERISTIC PERFORMANCE DATA





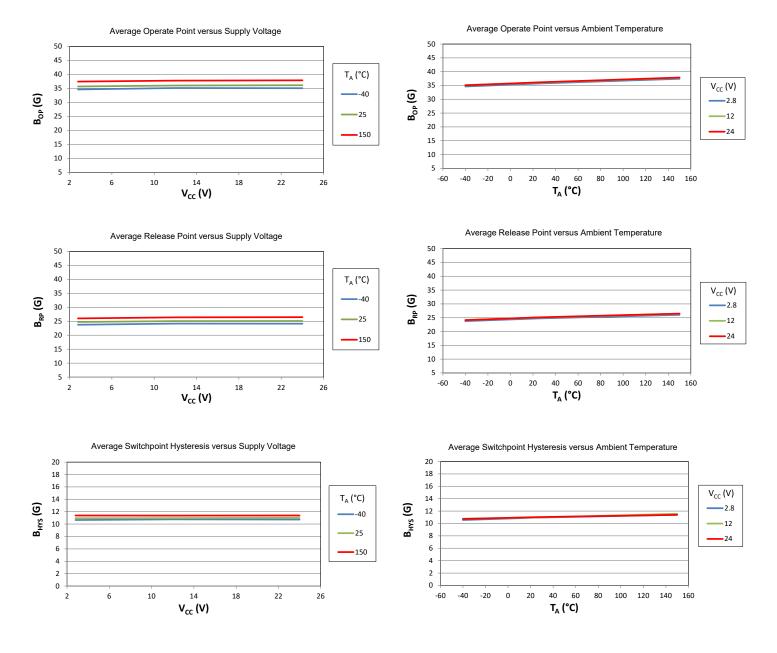


Average Low Output Voltage versus Ambient Temperature for  $\rm I_{OUT}$  = 20 mA





## CHARACTERISTIC PERFORMANCE DATA (continued)





## **High-Temperature Precision Hall-Effect Switch**

### FUNCTIONAL DESCRIPTION

#### OPERATION

The output of the APS11200 switches low (turns on) when a south-polarity magnetic field perpendicular to the Hall element exceeds the operate point threshold,  $B_{OP}$  (see Figure 2). After turn-on, the output voltage is  $V_{OUT(SAT)}$ . The output transistor is capable of continuously sinking up to 30 mA. When the magnetic field is reduced below the release point,  $B_{RP}$ , the device output goes high (turns off) to  $V_{OUTOFF}$ .

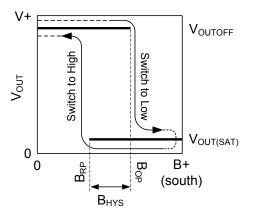


Figure 2: Device Switching Behavior

On the horizontal axis, the B+ direction indicates increasing south polarity magnetic field strength.

The difference in the magnetic operate and release points is the hysteresis,  $B_{HYS}$ , of the device. This built-in hysteresis allows clean switching of the output even in the presence of external mechanical vibration and electrical noise.

#### **POWER-ON BEHAVIOR**

Device power-on occurs once  $t_{ON}$  has elapsed. During the time prior to  $t_{ON}$ , and after  $V_{CC} \ge V_{CC}(min)$ , the output state is  $V_{OUT(SAT)}$ . After  $t_{ON}$  has elapsed, the output will correspond with the applied magnetic field for  $B > B_{OP}$  or  $B < B_{RP}$ . See Figure 3 for an example.

Powering-on the device in the hysteresis range (less than  $B_{OP}$  and higher than  $B_{RP}$ ) will give an output state of  $V_{OUTOFF}$ . The correct state is attained after the first excursion beyond  $B_{OP}$  or  $B_{RP}$ .

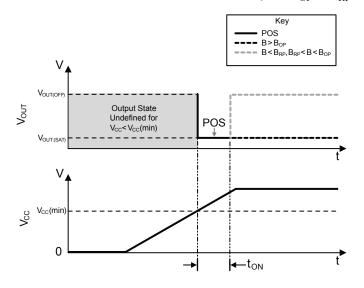


Figure 3: Power-On Sequence and Timing



## **High-Temperature Precision Hall-Effect Switch**

### **Functional Safety**

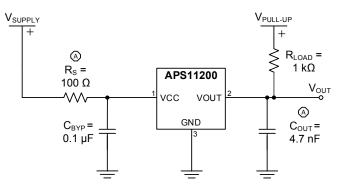
The APS11200 was designed in accordance with the international standard for automotive functional safety, ISO 26262. This product achieves an ASIL (Automotive Safety Integrity Level) rating of ASIL A

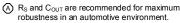
according to the standard. The APS11200 is classified as a SEooC (Safety Element out of Context) and can be easily integrated into safety-critical systems requiring higher ASIL ratings that incorporate external diagnostics or use measures such as redundancy. Safety documentation will be provided to support and guide the integration process. For further information, contact your local Allegro field applications engineer or sales representative.

### Applications

It is strongly recommended that an external bypass capacitor be connected (in close proximity to the Hall element) between the supply and ground of the device to guarantee correct performance under harsh environmental conditions and to reduce noise from internal circuitry. As is shown in Figure 1: Typical Application Circuit, a 0.1  $\mu$ F capacitor is required. In applications where maximum robustness is required, such as in an automobile, additional measures may be taken. In Figure 4: Enhanced Protection Circuit, a resistor in series with the VCC pin and a capacitor on the VOUT pin enhance the EMC immunity of the device. It is up to the user to fully qualify the Allegro sensor IC in their end system to ensure they achieve their system requirements.

These devices are sensitive in the direction perpendicular to the branded package face, and may be configured to sense magnetic





### Figure 4: Enhanced Protection Circuit

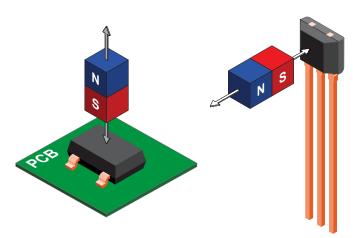
fields in a variety of orientations, such as the ones shown in Figure 5.

Extensive applications information for Hall-effect devices is available in:

- Hall-Effect IC Applications Guide, AN27701,
- Hall-Effect Devices: Guidelines for Designing Subassemblies Using Hall-Effect Devices AN27703.1
- Soldering Methods for Allegro's Products SMD and Through-Hole, AN26009

All are provided on the Allegro website:

#### www.allegromicro.com



**Figure 5: Sensing Configurations** 



## **High-Temperature Precision Hall-Effect Switch**

## **CHOPPER STABILIZATION**

A limiting factor for switchpoint accuracy when using Hall-effect technology is the small-signal voltage developed across the Hall plate. This voltage is proportionally small relative to the offset that can be produced at the output of the Hall sensor. This makes it difficult to process the signal and maintain an accurate, reliable output over the specified temperature and voltage range. Chopper stabilization is a proven approach used to minimize Hall offset.

The Allegro technique, dynamic quadrature offset cancellation, removes key sources of the output drift induced by temperature and package stress. This offset reduction technique is based on a signal modulation-demodulation process. Figure 6: Model of Chopper Stabilization Circuit (Dynamic Offset Cancellation) illustrates how it is implemented.

The undesired offset signal is separated from the magnetically induced signal in the frequency domain through modulation. The subsequent demodulation acts as a modulation process for the offset causing the magnetically induced signal to recover its original spectrum at baseband while the DC offset becomes a high-frequency signal. Then, using a low-pass filter, the signal passes while the modulated DC offset is suppressed. Allegro's innovative chopper stabilization technique uses a high-frequency clock. The high-frequency operation allows a greater sampling rate that produces higher accuracy, reduced jitter, and faster signal processing. Additionally, filtering is more effective and results in a lower noise analog signal at the sensor output. Devices such as the APS11200 that use this approach have an extremely stable quiescent Hall output voltage, are immune to thermal stress, and have precise recoverability after temperature cycling. This technique is made possible through the use of a BiCMOS process which allows the use of low-offset and low-noise amplifiers in combination with high-density logic and sample-and-hold circuits.

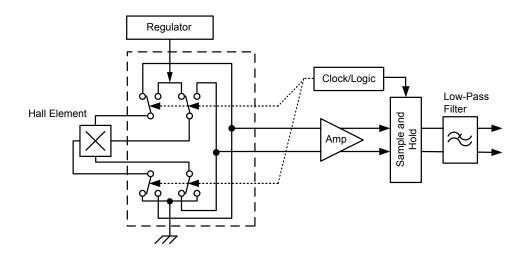


Figure 6: Model of Chopper Stabilization Circuit (Dynamic Offset Cancellation)



#### **POWER DERATING**

The device must be operated below the maximum junction temperature of the device,  $T_J(max)$ . Under certain combinations of peak conditions, reliable operation may require derating supplied power or improving the heat dissipation properties of the application. This section presents a procedure for correlating factors affecting operating  $T_J$ . (Thermal data is also available on the Allegro MicroSystems website.)

The Package Thermal Resistance,  $R_{\theta JA}$ , is a figure of merit summarizing the ability of the application and the device to dissipate heat from the junction (die), through all paths to the ambient air. Its primary component is the Effective Thermal Conductivity, K, of the printed circuit board, including adjacent devices and traces. Radiation from the die through the device case,  $R_{\theta JC}$ , is relatively small component of  $R_{\theta JA}$ . Ambient air temperature,  $T_A$ , and air motion are significant external factors, damped by overmolding.

The resulting power dissipation capability directly reflects upon the ability of the device to withstand extreme operating conditions. The junction temperature mission profile specified in the Absolute Maximum Ratings table designates a total operating life capability based on qualification for the most extreme conditions, where  $T_J$  may reach 175°C.

The silicon IC is heated internally when current is flowing into the VCC terminal. When the output is on, current sinking into the VOUT terminal generates additional heat. This may increase the junction temperature,  $T_J$ , above the surrounding ambient temperature. The APS11200 is permitted to operate up to  $T_J = 175^{\circ}$ C. As mentioned above, an operating device will increase  $T_J$  according to equations 1, 2, and 3 below. This allows an estimation of the maximum ambient operating temperature.

$$P_D = V_{IN} \times I_{IN} \tag{1}$$

$$\Delta T = P_D \times R_{\theta,JA} \tag{2}$$

$$T_J = T_A + \Delta T \tag{3}$$

For example, given common conditions such as:  $T_A = 25^{\circ}C$ ,  $V_{CC} = 12 \text{ V}$ ,  $I_{CC} = 2 \text{ mA}$ ,  $V_{OUT} = 185 \text{ mV}$ ,  $I_{OUT} = 20 \text{ mA}$  (output on), and  $R_{\theta JA} = 165^{\circ}C/W$ , then:

$$P_D = (V_{CC} \times I_{CC}) + (V_{OUT} \times I_{OUT}) = (12 \ V \times 2 \ mA) + (185 \ mV \times 20 \ mA) = 24 \ mW + 3.7 \ mW = 27.7 \ mW$$

$$\Delta T = P_D \times R_{\theta JA} = 27.7 \ mW \times 165^{\circ}C/W = 4.6^{\circ}C$$

$$T_J = T_A + \varDelta T = 25^{\circ}C + 4.6^{\circ}C = 29.6^{\circ}C$$

A worst-case estimate,  $P_D(max)$ , represents the maximum allowable power level ( $V_{CC}(max)$ ,  $I_{CC}(max)$ ), without exceeding  $T_J(max)$ , at a selected  $R_{\theta JA}$ .

For example, given the conditions  $R_{0JA} = 228^{\circ}C/W$ ,  $T_J(max) = 175^{\circ}C$ ,  $V_{CC}(max) = 24$  V,  $I_{CC}(max) = 4$  mA,  $V_{OUT} = 500$  mV, and  $I_{OUT} = 25$  mA (output on), the maximum allowable operating ambient temperature can be determined.

The power dissipation required for the output is shown below:

$$P_D(V_{OUT}) = V_{OUT} \times I_{OUT} = 500 \text{ mV} \times 25 \text{ mA} = 12.5 \text{ mW}$$

The power dissipation required for the IC supply is shown below:

$$P_D(V_{CC}) = V_{CC} \times I_{CC} = 24 V \times 4 mA = 96 mW$$

Next, by inverting using equation 2:

$$\Delta T = P_D \times R_{\theta JA} = [P_D(V_{OUT}) + P_D(V_{CC})] \times 228^{\circ}C/W =$$

$$(12.5 \ mW + 96 \ mW) \times 228^{\circ}C/W =$$

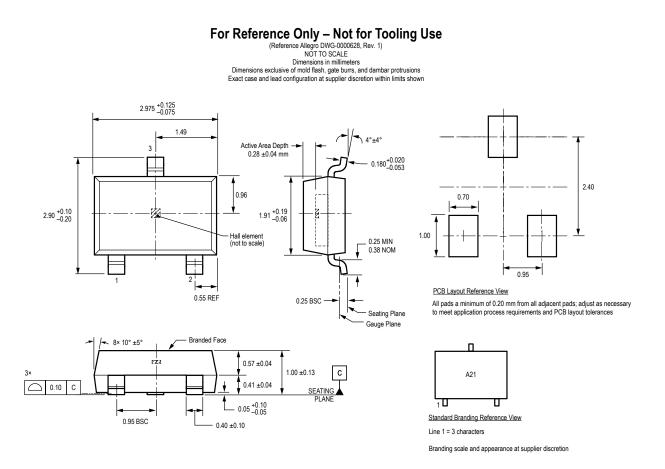
$$108.5 \ mW \times 228^{\circ}C/W = 24.7^{\circ}C$$

Finally, by inverting equation 3 with respect to voltage:

$$T_A(est) = T_J(max) - \Delta T = 175^{\circ}C - 24.7^{\circ}C = 150.3^{\circ}C$$

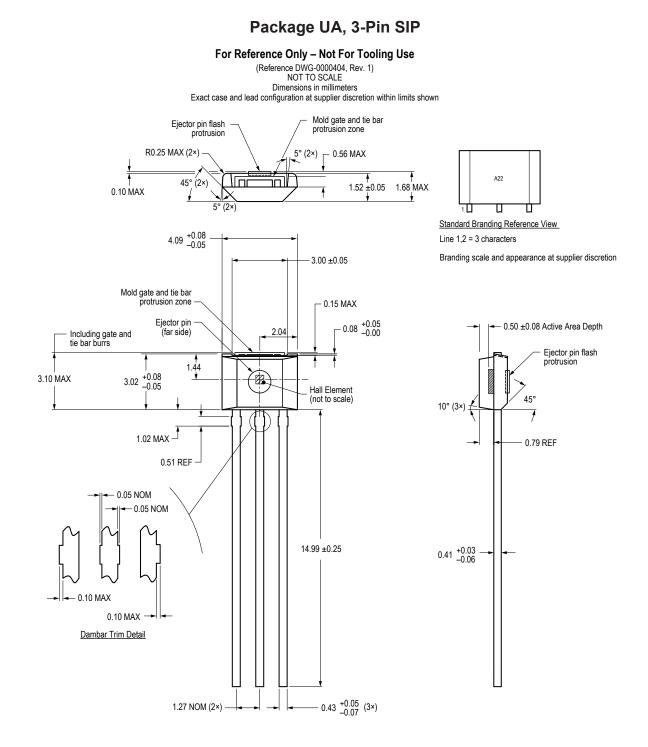
In the above case, there is sufficient power dissipation capability to operate up to  $T_A(est)$ . The example indicates that  $T_A(max)$  can be as high as 150.3°C without exceeding  $T_J(max)$ . However, the  $T_A(max)$  rating of the device is 150°C; the APS11200 performance is not guaranteed above  $T_A = 150$ °C.

## Package LH, 3-Pin (SOT-23W)





## **High-Temperature Precision Hall-Effect Switch**





#### **Revision History**

Number	Date	Description
-	February 23, 2018	Initial release
1	January 16, 2019	Minor editorial updates
2	January 22, 2020	Minor editorial updates
3	January 31, 2022	Updated package drawings (pages 12-13)

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